



TECHNISCHE  
UNIVERSITÄT  
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Mihir Joshi

## **Development of semi-actively damped milling chuck for chatter reduction in high dynamic milling**

**Schriftenreihe des PTW  
„Innovation Fertigungstechnik“**

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# Development of semi-actively damped milling chuck for chatter reduction in high dynamic milling

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## Greek letters and other symbols

Variable	Unit	Description
$A_{sp}$	$mm^2$	uncut chip cross-section
$\mathbf{C}$	-	damping matrix
$D$	-	damping co-efficient according to LEHR
$D_{opt}$	-	optimal damping ratio
$E$	-	modulus of elasticity
$F$	N	force
$F(\omega)$	-	force matrix in frequency domain
$F_a$	N	active cutting force
$F_x$	N	measured force in x-direction
$F_y$	N	measured force in y-direction
$G(\omega)$	-	compliance matrix in frequency domain
$I$	$mm^4$	Area moment of inertia
$I_A$	$mm^4$	Area moment of inertia about a particular axis

*List of Tables*

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Variable	Unit	Description
$I_c$	A	electric current
$\mathbf{K}$	-	stiffness matrix
$\mathbf{M}$	-	mass matrix
$Q$	$cm^3$	material removal rate
$R_m$	$N/m^2$	ultimate tensile strength
$U$	-	uniformity ratio
$X$	m	displacement matrix
$X(\omega)$	-	displacement matrix in frequency domain
$X_0$	-	maximum amplitude
$dot{X}$	m/s	velocity matrix
$\ddot{X}$	$m/s^2$	acceleration
$a_{cr}$	mm	critical axial depth of cut
$a_e$	mm	radial depth of cut
$a_p$	mm	axial depth of cut
$b$	-	damping constant
$b_{lim}$	mm	maximum depth of cut
$c$		damping co-efficient
$d_i$	mm	diameter
$f_0$	Hz	eigen-frequency
$f_z$	mm	feed per cutting edge
$h_c$	mm	uncut chip thickness
$i$	-	imaginary number
$l_c$	mm	cutting edge contact length
$l_i$	mm	length
$k$	N/m	stiffness
$m$	kg	mass
$m_{va}$	kg	mass of vibration absorber
$n_i$	1/s	natural frequencies
$r_T$	mm	cutting tool radius
$t$	s	time
$v_c$	m/min	cutting speed
$v_f$	m/min	feed speed

---

Variable	Unit	Description
$\dot{x}$	m/s	velocity
$\ddot{x}$	$m/s^2$	acceleration
$x$	m	displacement
$\alpha_i$	°	relief angle
$\beta_i$	°	wedge angle
$\gamma_i$	°	rake angle
$\lambda$	°	helix angle
$\mu_A$	-	mass ratio
$\mu_T$	-	mass ratio
$\tau_0$	$N/m^2$	shear stress
$\tau_i$	°	pitch angle
$\omega_0$	rad/s	first eigen(circular) frequency

---

## Symbols and Abbreviations

### Abbreviations

HSC	High-Speed-Cutting, Hochgeschwindigkeitsbearbeitung
ISO	International Standards Organisation
DIN	Deutsches Institut für Normung / German institute for standardisation
EN	English
SK	Steilkegel / for taper shank
HSK	Hohlschaftkegel / for hollow taper shank
HPC	High-Performance-Cutting, Hochleistungsbearbeitung
ERF	Electro-rheological fluid
MRF	Magneto-rheological fluid
DVA	Dynamic vibration absorber
SLD	Stability lobe diagram
HB	Brinell Hardness
HRC	Rockwell hardness constant
CNC	Computerised numerical control

NC	Numerical control
FFT	Fourier frequency transformation
BNC	Bayonet Neill–Concelman
PCB	printed circuit board

## Preface by the editor

Der Einsatz von Zerspanungswerkzeugen zur Bearbeitung von Formen und Gesenken mit einem größtmöglichen Produktivitätsgewinn steht seit Jahrzehnten im Mittelpunkt der Forschung. Dieses Thema ist für Hochlohnländer von strategischer Bedeutung, um wettbewerbsfähig zu bleiben. Die Werkzeugsysteme, bestehend aus Werkzeugen und Spannfuttern insbesondere bei einem großen Aspektverhältnis, stellen das schwächste Glied in der Konstruktion der Werkzeugmaschine dar. Wodurch die einsetzbare Schnittgeschwindigkeit Aufgrund Rattern signifikant eingeschränkt wird.

Ziel dieser Arbeit ist daher die Entwicklung eines semi-aktiv gedämpften Spannfutters zur Reduzierung von Rattern. Zunächst wurden die Randbedingungen des bestehenden Spannfutters mittels Modalanalyse ermittelt. Anschließend wurden die Grenzen des Prozesses für das bestehende Fräsfutter experimentell untersucht. Bei der Konstruktion des Prototyps wird die Produktentwicklungsmethodik nach der VDI-Richtlinie 2221 angewendet. Elektrorheologische Flüssigkeiten ändern ihre Viskosität, wenn sie durch ein elektrisches Feld aktiviert werden. Die Anpassung des bestehenden Werkzeugsystems für die Integration von elektrorheologischen Flüssigkeiten wird in zwei Hauptaspekten gegliedert. Erstens die Konstruktion eines Massenrings, der mit Hilfe der elektrorheologischen Flüssigkeit an das Fräsfutter zur Schwingungsdämpfung gekoppelt wurde. Die Konstruktion des Massenrings wurde iterativ durch Experimente bestimmt. Zweitens die Integration der Möglichkeit zur Übertragung der elektrischen Spannung beim Fräsen. Die größte Herausforderung besteht hier darin, eine stabile Spannungsübertragung in das rotierende System zu ermöglichen. Die Validierung des Prototyps wurde durch Schwingungsanalyse durchgeführt. Durch Fräsexperimente wurde die Anwendung des entwickelten Prototyps für einen Anwendungsfall demonstriert.

Darmstadt, im Januar 2022

Prof.Dr.-Ing. Eberhard Abele

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