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Confinement Induced Segregation Effects  
in Suspension Rheology

Sven Pieper



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5

# **Confinement Induced Segregation Effects in Suspension Rheology**

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*A gazelle is just a giraffe,  
plotted logarithmically.*

- SMBC, Z. Weinermith



## **Abstract**

The formation of a particle depleted and a structured particle layer adjacent to a confining surface is a well known effect in suspension rheology. This thesis aimed to provide insight into specific properties of these layers. Firstly, the influence of pressure on the depleted layer, which is the cause of apparent wall slip, should be quantified. A slit die was fitted with pressure transducers and an outlet restrictor. By performing experimental work as well as simulations, it was demonstrated that the pressure's influence is negligible. Secondly, a setup should be provided, which allows for the characterization of both depleted and structured layers with regard to various, independently variable, parameters. To this end, a parallel plate rheometer was modified for optical accessibility. Optical velocimetric and concentration determination methods were implemented. After carefully mapping the modification induced distortion of the velocity field, concentration profiles were obtained and analyzed. Especially the demonstrated vertical concentration gradient poses a new challenge for rheology.

## **Kurzdarstellung**

In der Rheologie von Suspensionen wird beobachtet, dass sich durch die Anwesenheit von begrenzenden Oberflächen partikelverarme und strukturierte Partikelsschichten bilden. Diese Arbeit beschäftigt sich mit den Eigenschaften dieser Schichten und den Folgen für die Rheologie. Dabei wurden im Wesentlichen zwei Ziele verfolgt. Erstens, den Einfluss des Druckes auf die partikelverarme Gleitschicht, als Ursache des scheinbaren Wandgleitens, zu quantifizieren. Zu diesem Zweck wurde eine Schlitzdüse mit Druckaufnehmern sowie Auslassdrossel versehen und verschiedene simulative wie experimentelle Untersuchungen durchgeführt. Hierbei konnte nachgewiesen werden, dass der absolute Druck keinen Einfluss auf das scheinbare Gleiten hat. Zweitens, einen Aufbau bereitzustellen, der es ermöglicht die Eigenschaften der verarmten Fluidschicht und der Partikellagen als Funktion verschiedener, von einander unabhängiger, Größen zu untersuchen. Hierzu wurde eine Platte-Platte Rheometer für optische Zugänglichkeit modifiziert und optische Strömungs- und Konzentrationsmessverfahren implementiert. Nach der ausführlichen Charakterisierung der auftretenden Verzerrung des Geschwindigkeitsfeldes konnten Konzentrationsfelder abgebildet und einige Analysen durchgeführt werden. Insbesondere der Nachweis eines vertikalen Konzentrationsgradienten stellt die Rheologie vor neue Herausforderungen.



## List of Publications

### Articles in Peer-Reviewed Journals and Conference Proceedings

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PIEPPER S., SCHMID H.-J.: Guard ring induced distortion of the steady velocity profile in a parallel plate rheometer. *Appl. Rheol.* **26** (2016) 64533

PIEPPER S., SCHMID H.-J.: Layer-formation of non-colloidal suspensions in a parallel plate rheometer under steady shear. *J. Non-Newtonian Fluid Mech.* **234** (2016) 1-7

PIEPPER S., KIRCHHOFF N., SCHMID H.-J.: Absence of pressure sensitivity of apparent wall slip in pressure-driven flow of non-colloidal suspensions. *Rheol. Acta* **54** (2015) 69-75

PIEPPER S., SCHMID H.-J.: Apparent wall slip and particle migration in laminar flow of suspensions through a slit die. *Proceeding: PARTEC - International Congress on Particle Technology*, Nuremberg, Germany (2013)

### Oral and Poster Presentations

---

PIEPPER S., SCHMID H.-J.: Einfluss von Begrenzungsringen am Umfang auf die Geschwindigkeitsprofile von Suspensionen im Platte-Platte Rheometer. *Gemeinsame Diskussionstagung der Deutschen Rheologischen Gesellschaft (DRG) und der Process-Net Fachgruppe "Rheologie"*, Berlin, Germany (2016)

PIEPPER S., SCHMID H.-J.: Direct observation of velocity fields of concentrated suspensions and formation of wall adjacent particle organization in a PP rheometer via PIV. *AERC - Annual European Rheology Conference*, Nantes, France (2015)

PIEPPER S., SCHMID H.-J.: Direkte Beobachtung von Geschwindigkeitsfeldern konzentrierter Suspensionen in Platte-Platte Rheometern mittels PIV. *Jahrestreffen der Fachgruppe "Rheologie"*, Ludwigshafen am Rhein, Germany (2015)

PIEPPER S., SCHMID H.-J.: Direct obervation of a suspension's time dependent apparent wall slip in a plate-plate rheometer. *AERC - Annual European Rheology Conference*, Karlsruhe, Germany (2014)

PIEPPER S., SCHMID H.-J.: Entwicklung von scheinbarem Wandgleiten unter dem Einfluss verschiedener Fließparameter. *Jahrestreffen der Fachgruppe "Rheologie"*, Magdeburg, Germany (2013)

PIEPPER S., KIRCHHOFF N., SCHMID H.-J.: Relationship between apparent wall slip and the pressure gradient along a slit die. *ICR - International Congress on Rheology*, Lisbon, Portugal (2012)



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## Abbreviations and Symbols

CP	cone plate
CPP	cone partitioned plate
HPCR	high pressure capillary rheometer
NaI-PTX	refractive index and density matching fluid, mixture of aqueous sodium iodide solution, PEG 400 and Triton X100
PDMS	poly(dimethylsiloxane)
PEG	Polyethylene glycol / poly(ethylene oxide)
PIV	particle image velocimetry
PMMA	poly(methyl methacrylate)
PP	rotating parallel plate
SD	standard deviation
<i>Pe</i>	Peclet number
$\Delta$	difference
$\Delta R$	radii difference, $\Delta R = R_a - R$
$\Delta p_0$	nominal pressure difference
$\Delta p_{max}$	maximum pressure difference
$\Delta p_{total}$	total pressure drop between first and last transducer
$\delta$	slip layer thickness
$\eta$	dynamic viscosity
$\eta_0$	dynamic viscosity of the matrix fluid
$\eta_s$	dynamic viscosity of the suspension
$[\eta]$	intrinsic viscosity
$\dot{\gamma}$	shear rate

$\dot{\gamma}_W$	shear rate at the wall
$\dot{\gamma}_{ap,s}$	apparent shear rate at the wall, slip corrected
$\dot{\gamma}_{ap}$	apparent shear rate at the wall
$\dot{\gamma}_{r=R}$	nominal shear rate at the edge of the rotating plate
$\gamma$	shear deformation
$\lambda$	wavelength / direction parameter
$\lambda_c$	cut-off wavelength
$\mu$	expected value / position parameter
$\omega$	angular velocity
$\bar{\phi}$	mean particle volume fraction of the sample
$\bar{\phi}_T$	mean tracer particle volume fraction of the sample
$\bar{\phi}_{56}$	gap mean detected particle volume fraction, $\bar{\phi} = 56\%$
$\phi$	volume fraction
$\phi_T$	volume fraction of tracer particles
$\phi_m$	maximum loose packing particle volume fraction
$\phi_{T,m}$	maximum packing tracer particle volume fraction
$\Sigma_p$	particle stress contribution
$\sigma$	standard deviation / edge parameter
$\tau$	shear stress
$\tau_W$	shear stress at the wall
$\tau_{ap}$	apparent shear stress at the edge of the rotating plate
$\tau_{r=R}$	shear stress at the edge of the rotating plate
$\vartheta$	temperature on the Celsius scale
$A$	area / scaling parameter
$A_{ow}$	area of the observation window
$F$	force / cumulative normal distribution function
$F_R$	contribution matrix of radius $R$
$H$	gap / slit height

$H_{max}$	maximum gap height of the parameter set
$H_{nom}$	nominal gap height
$H_{opt}$	gap height from optical measurement
$I$	light intensity
$I_0$	reference light intensity
$I_{max}$	maximum light intensity
$\bar{I}$	mean intensity
$K_\eta$	viscosity parameter
$K_c$	collision parameter
$L$	slit length / distance from the light sheet lens
$M$	torque
$O_R$	orientation projection image of radius $R$
$Q$	volumetric flow rate
$Q_3$	cumulative fraction by volume
$Q_{shear}$	volumetric flow rate due to shear flow
$Q_s$	volumetric flow rate due to slip
$Q_{total}$	total volumetric flow rate
$R$	radius of the rotating plate / radius to be considered
$R_a$	inner radius of the guard ring
$S$	camera sled position
$T$	absolute temperature
$U$	chrominance, blue component
$V$	chrominance, red component
$W$	slit width
$Y$	luminance component (perceived brightness)
$d_{target}$	diameter corresponding to target step
$K$	curvature parameter
$\bar{a}$	mean visible particle radius

$a$	particle radius
$b$	light sheet thickness
$d$	diameter / darkness parameter
$d_{10}$	equivalent diameter of the 10th percentile
$d_{50}$	equivalent diameter of the 50th percentile, median diameter
$d_{90}$	equivalent diameter of the 90th percentile
$f_s$	settling hindrance function
$h$	vertical coordinate
$k_1, k_2$	lens distortion parameters
$k_B$	Boltzmann constant
$k_s$	slope parameter
$m$	Krieger-Dougherty exponent
$\bar{n}$	mean number density
$n$	number density
$\mathbf{n}$	surface normal vector
$n_D$	refractive index, $\lambda = 589.29 \text{ nm}$
$n_{D20}$	refractive index at $\vartheta = 20.0^\circ \text{ C}$ , $\lambda = 589.29 \text{ nm}$
$g$	brightness gradient vector
$p$	pixel coordinates
$p$	pressure
$p_a$	affected pixel coordinates
$r$	radial distance coordinate
$s$	displacement
$t$	time
$\bar{v}$	mean velocity over the cross section
$\mathbf{v}$	velocity vector
$v$	circumferential velocity / velocity
$v_0$	macroscopic relative velocity
$v_s$	slip velocity

$w$	weight fraction
$x, y, z$	coordinates
$\hat{x}, \hat{y}$	distorted coordinates
$x_c, y_c$	central coordinates of the image