Direct Torque Control of Permanent Magnet Synchronous Machine

Von der Fakultät für Elektrotechnik und Informationstechnik der Universität der Bundeswehr München

zur Erlangung des akademischen Grades eines Doktor-Ingenieur (Dr.-Ing.)

genehmigte Dissertation

von

M. Sc. Yaohua Li



Neubiberg 2010

Vorsitzender: Prof. Dr. G. Bauch
1. Berichterstatter: Prof. Dr. D. Gerling
2. Berichterstatter: Prof. Dr. C. Hillermeier

Tag der Promotion: 15.09.2010

Forschungsberichte Elektrische Antriebstechnik und Aktorik

Band 8

Yaohua Li

Direct Torque Control of Permanent Magnet Synchronous Machine

Shaker Verlag Aachen 2010

Bibliographic information published by the Deutsche Nationalbibliothek

The Deutsche Nationalbibliothek lists this publication in the Deutsche Nationalbibliografie; detailed bibliographic data are available in the Internet at http://dnb.d-nb.de.

Zugl.: München, Univ. der Bundeswehr, Diss., 2010

Copyright Shaker Verlag 2010
All rights reserved. No part of this publication may be reproduced, stored in a retrieval system, or transmitted, in any form or by any means, electronic, mechanical, photocopying, recording or otherwise, without the prior permission of the publishers.

Printed in Germany.

ISBN 978-3-8322-9511-0 ISSN 1863-0707

Shaker Verlag GmbH • P.O. BOX 101818 • D-52018 Aachen Phone: 0049/2407/9596-0 • Telefax: 0049/2407/9596-9

Internet: www.shaker.de • e-mail: info@shaker.de

To my parents,

Xiang Li and Xiping Cao

Abstract

Abstract

This thesis presents the direct torque control (DTC) on the permanent magnet synchronous machine (PMSM). The effects of zero voltage vectors and non-zero voltage vectors on the PMSM DTC drive are analyzed. New switching tables are developed. The control of the amplitude of stator flux, torque angle and torque of the PMSM DTC drive are discussed. The voltage vector selection strategy of the PMSM DTC drive is given. All of these are verified by simulation and experimental results.

Due to the voltage drop on stator resistance and the move of rotor flux vector the application of zero voltage vectors decreases the amplitude of stator flux and torque. Thus the use of zero voltage vectors to increase the amplitude of stator flux and decrease torque can't satisfy the control of stator flux. For the PMSM, the application of zero voltage vectors can't produce the negative torque. When the PMSM operates as a brake, the use of zero voltage vectors introduces stator current ripple. Based on the effect of zero voltage vectors, a switching table using zero voltage vectors for the PMSM DTC drive is proposed and the advantages of the use of zero voltage vectors are given.

The switching table of the PMSM DTC drive is based on the viewpoint that the change of torque is always consistent with the change of torque angle. It holds true only at the dynamic state. When the PMSM DTC drive is at the steady state, the effect of the change of the amplitude of stator flux on torque can't be neglected comparing with the change of torque angle. When torque angle is higher, the change of torque isn't always consistent with the change of torque angle and the switching table causes torque ripple. Using the three-phase and two-phase connection, a two-level voltage source inverter (VSI) can generate 12 non-zero voltage vectors of 30° between each other. And we divide voltage vector plane into 12 sectors of 30° between each other. Thus there are 12 nonzero voltage vectors to be used in every sector. Based on the effect of these voltage vectors on torque in a sector, the PMSM DTC drive should select V_{120°} to decrease the amplitude of stator flux and increase torque and select $V_{300^{\circ}}$ to increase the amplitude of stator flux and decrease torque. A novel switching table for the PMSM DTC drive is proposed. Simulation results show the novel switching table can suppress torque ripple comparing with the conventional switching table, but when torque angle is higher, it will also cause torque ripple. In simulation the commutation torque ripple due to the additional use of the twophase connection is neglected, but experimental results show it degrades the control performance in practice.

II Abstract

As the DTC is the hysteresis control, the voltage vector selection strategy as the hysteresis control rule is essential to the control performance. The control of the amplitude of stator flux, torque angle and torque of PMSM are shown in the following. For the control of the amplitude of stator flux, if the angle between stator flux vector and the applying voltage vector is within (-90°, 90°), the voltage vector increases the amplitude of stator flux and if the angle is within (90°, 270°), the voltage vector decreases the amplitude of stator flux. For the control of torque angle, if the angle between stator flux vector and the applying voltage vector is within (0°, 180°), the voltage vector increases torque angle and if the angle is within (180°, 360°), the voltage vector decreases torque angle. For the control of torque of SPMSM, if the angle between rotor flux vector and the applying voltage vector is within (0°, 180°), the voltage vector increases torque and if the angle is within (180°, 360°), the voltage vector decreases torque. For the control of torque of PMSM, if the angle between stator flux vector and the applying voltage vector is within $(\lambda - \theta, 180^{\circ} + \lambda - \theta)$, the voltage vector increases torque and if the angle is within $(180^{\circ}+\lambda-\theta, 360^{\circ}+\lambda-\theta)$, the voltage vector decreases torque. The effect of voltage vector on the amplitude of stator flux, torque angle and torque of PMSM is proportional to the amplitude of voltage vector and the applying period. The voltage vector selection area of the PMSM DTC drive and a simplified voltage vector selection strategy are given. The technology of space vector modulation (SVM) is used to generate the applying voltage vector. Comparing with the PMSM DTC drive using the switching table. the voltage vector selection strategy and the SVM are used to generate the switching signals instead of the switching table and the continuous stator flux position and torque angle information instead of stator flux sector information are needed. Simulation and experimental results show comparing with the switching table, the voltage vector selection strategy can decrease the ripples in stator current and torque, fix the switching frequency of the VSI and the PMSM DTC drive can work at higher load situation.

Two methods to start the PMSM FOC/DTC drive are discussed. The two-step pre-fixed method is easy to implement, but as the rotation direction is arbitrary when the rotor is fixed to the given position, it can't be used in some applications. The SPWM open-loop control method is an easy way to start the motor, but it will increase the calculation burden to implement the SPWM control and for the DTC using the voltage model to estimate stator flux, it will introduce the vibration when the DTC is switched on to control the motor.

Acknowledgements

This research work has been carried out during the years 2007-2010 in the Institute for Electrical Drives and Actuators of University of Federal Defence Munich.

Firstly, I wish to express my sincere thanks to my supervisor, Prof. Dr.-Ing. Dieter Gerling, for his valuable guidance, great patience and wisdom throughout my research activities. His inspiring guidance and encouragement have been of enormous significance to me.

I would like to express my thanks to Prof. Weiguo Liu, for his great support and valuable advice to my study.

I wish to express my gratitude to the committee of this thesis, Prof. Dr.-Ing. G. Bauch and Prof. Dr.-Ing. C. Hillermeier for their support and advice.

Here I wish to send my warmest thanks to all of my colleagues for giving me much help. Special acknowledgements are given to Dr.-Ing. Gurakuq Dajaku and Dr.-Ing. Harald Hofmann for their helps and suggestions. I also would like to thank Dr.-Ing. Hans-Joachim Köbler, Dr.-Ing. Benno Lange, Dr.-Ing. Berthold Schinnerl, Dipl.-Ing. Rainer Hildebrand, Dipl.-Ing. Oliver Benjak, Dipl.-Ing. Fatmir Hetemi, Dipl.-Ing. Xhevat Dajaku, Dipl.-Ing. Johannes Klötzl, Dipl.-Ing. Ulf Kreutzer, Dipl.-Ing. Christian Laudensack, Dipl.-Ing. Klaus Mühlbauer, Dr.-Ing. Marcin Pyc, Dipl.-Ing. Jens Richter, Dipl.-Ing. Johann S. Mayer, M. Sc. Nizar Khateeb, M. Sc. Qiang Yu and Ph. D. Lixin Tang.

In addition, I would like to thank the Chinese Scholarship Council for granting me the highly competitive scholarship and the Institute for Electrical Drives and Actuators of University of Federal Defence Munich and Forschungszentrum für Elektrische Antriebstechnik und Aktorik München GmbH (FEAAM) for giving me the financial support during my study in Germany.

Finally, I am deeply indebted to my father Xiang Li and my mother Xiping Cao for their love and support during my study in Germany.

Neubiberg, 2010

Yaohua LI

Contents i

Contents

Chapter 1	1
1.1 Background	1
1.2 Permanent magnet synchronous motor	1
1.2.1 SPMSM	
1.2.2 IPMSM	4
1.3 The control schemes	
1.4 The description of test bench	6
1.5 Outline of this thesis	
Chapter 2	10
2.1 The v/f control	10
2.1.1 Introduction	10
2.1.2 The SPWM	10
2.1.3 The phase circuit of PMSM	11
2.1.4 Experimental results for the v/f control	12
2.1.4.1 The SPMSM	12
2.1.4.2 The IPMSM	14
2.2 The FOC	
2.2.1 The concept of FOC	15
2.2.2 The implementation of the PMSM FOC drive	
2.2.2.1 The FOC using the SPWM	17
2.2.2.2 The FOC using the hysteresis current control	20
2.3 Conclusion	
Chapter 3	27
3.1 Introduction	27
3.2 The PMSM DTC drive	27
3.2.1 The concept of DTC for the PMSM	27
3.2.2 The condition of DTC	30
3.2.3 The control of stator flux	31
3.2.4 The switching table	34
3.2.5 The implementation of the PMSM DTC drive	35
3.3 Simulation results	37
3.4 Experimental results	41
3.4.1 The SPMSM	41
3.4.1.1 The current model	41

ii Contents

3.4.1.2 The voltage model	43
3.4.2 The IPMSM	44
3.4.2.1 The current model	44
3.4.2.2 The voltage model	
3.5 Conclusion	
Chapter 4	
4.1 Introduction	
4.2 The effect of zero voltage vectors	47
4.3 The switching table for the IM DTC drive	50
4.3.1 The switching table	50
4.3.2 The SPMSM	
4.3.3 The IPMSM	52
4.3.4 Analysis of the switching table for the IM DTC drive	54
4.4 The switching table using the zero voltage vectors	
4.4.1 The switching table	54
4.4.2 The SPMSM	55
4.4.2 The IPMSM	56
4.5 Experimental results	58
4.5.1 The SPMSM	58
4.5.1.1 The switching table for the PMSM DTC drive	58
4.5.1.2 The switching table for the IM DTC drive	60
4.5.1.3 The switching table using zero voltage vectors	
4.5.2 The IPMSM	62
4.5.2.1 The switching table for the PMSM DTC drive	62
4.5.2.2 The switching table for the IM DTC drive	64
4.5.2.3 The switching table using zero voltage vectors	66
4.5.3 Analysis of experimental results	67
4.6 The advantages of the use of zero voltage vectors	68
4.7 Conclusion	
Chapter 5	69
5.1 Introduction	69
5.2 12 non-zero voltage vectors	71
5.3 The novel switching table	
5.3.1 The switching table	84
5.3.2 The SPMSM	
5.3.3 The IPMSM	86
5.4 Experimental results	
5.4.1 The SPMSM	

5.4.2 The IPMSM	90
5.5 The conclusion	92
Chapter 6	94
6.1 Introduction	94
6.2 The control of the amplitude of stator flux	94
6.3 The control of torque angle	98
6.4 The control of torque	
6.4.1 The SPMSM	100
6.4.2 The IPMSM	104
6.6 The voltage vector selection area	110
6.6 The voltage vector selection strategy	113
6.7 A simplified voltage vector selection strategy	114
6.8 The SVM	116
6.8 Simulation results	117
6.8.1 The SPMSM	117
6.8.2 The IPMSM	119
6.9 Experimental results	120
6.9.1 The switching table	121
6.9.2 The voltage vector selection strategy	122
6.10 Conclusion	
Chapter 7	126
7.1 Introduction	126
7.2 The two-step pre-fixed method	126
7.2.1 The FOC	127
7.2.2 The DTC	128
7.2.2.1 The current model	128
7.2.2.2 The voltage model	128
7.3 The SPWM open-loop control method	129
7.3.1 The FOC	129
7.3.2 The DTC	130
7.3.2.1 The current model	130
7.3.2.2 The voltage model	131
7.4 Conclusion	132
Chapter 8	133
8.1 Conclusions	133
8.2 Future work	137
References	138
List of symbols and acronyms	142